

Influence of Cutting Parameters on Turning Process Using Anova Analysis

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Available online at: www.isca.in

Received 30th August 2013, revised 10th September 2013, accepted 23rd September 2013

Abstract

In a turning process surface roughness depend on machining parameters and tool geometry. In this work considering three machining parameters and two tool geometrical parameters 243 experiments were conducted for full factorial design. Using ANOVA analysis the influence of these parameters on surface roughness was studied.

Keywords: Optimization, machining parameters, ANOVA, rake angles, surface finish.

Introduction

In Single pass turning the conditions during cutting such as cutting speed, feed rate and depth of cut should be selected to optimize the surface roughness. The selection to efficient machining parameters such as machining speed, feed rate and depth of cut has a direct impact in the metal cutting processes. The cutting tool geometry such as back rake, side rake also slightly affects the surface roughness.

The major efforts of earlier works were concentrated on optimization of machining parameters and not concentrated on geometry of cutting. In this work we tried to find influence of machining parameters and tool geometry on surface roughness.

Machining parameters in turning process: In metal cutting, there are many factors related to process planning for machining operations. These factors can be classified as: i. Type of machining operations (turning, facing, milling, etc.), ii. Parameters of machine tools (rigidity, horse power, etc.), iii. Parameters of cutting tools (material, geometry, etc.), iv. Parameters of cutting conditions (cutting speed, feed rate, depth of cut, etc.), v. Characteristics of work pieces (material, geometry, etc.).

Among these factors cutting parameters (speed, feed rate and depth of cut) and tool geometry (back rake, side rake) are evidently dominating ones in a machining operation.

Cutting Speed (v): The cutting speed of a tool is the speed at which the metal is removed by the tool from the work material. In a lathe it is the peripheral speed of the work part in m/min.
 $V = \pi DN/1000$ (m/min)

Where D, N are diameter of work piece (mm) and cutting speed (rpm) respectively.

Feed (f): The feed of the cutting tool in lathe work is the distance, the tool advances for each revolution of the work piece in mm.

Depth of cut (d): The depth of cut is the perpendicular distance measured from the machined surface to the uncut surface of the work piece in mm.

Back rake angle: It is the angle provided from the cutting edge to the shank of a single point cutting tool, back rake is to help control the direction of the chip, which naturally curves into the work due to the difference in length from the outer and inner parts of the cut. It also helps counteract the pressure against the tool from the work by pulling the tool into the work piece.

5. Side rake angle: It is the angle provided between front face to the side of the single point cutting tool.

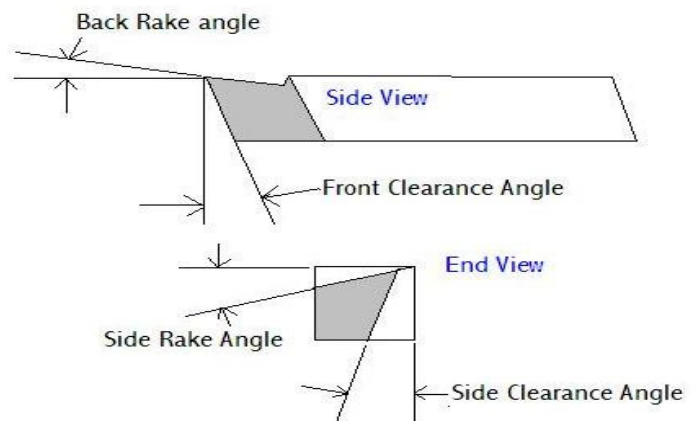


Figure-1

Two rake angles of single point cutting tool

Side rake along with back rake controls the chip flow and partly counteracts the resistance of the work to the movement of the cutter and can be optimized to suit the particular material being cut.

For a given machining operation determination of the optimum cutting conditions involves a conflict between maximizing the material removal rate and minimizing the surface roughness. The machining process optimization is to determine the most advantageous cutting condition. This is to determine optimal machining parameters such as v (cutting speed), f (feed rate), d (depth of cut) and the tool geometry back rake, side rake to optimize specified objectives such as surface roughness and MRR.

Literature-Survey: Gilbert¹ optimized of machining parameters in turning operation by considering maximum production rate and minimum production as objective functions. By expressing the production cost and production rate in terms of speed and feed rate Armarego and Brown² and partially differentiating these terms with respect to speed and feed and equating to zero the optimum cutting conditions are obtained. Brewer and Rueda³ obtained number of nomograms for facilitating the determination of the economic machining conditions by employing the criterion of reducing the machining cost to a minimum for cast iron and steels. The usage of geometric programming for selection of machining variables were studied by Walvekar and Lambert⁴ and obtained optimized cutting speed and feed rate to optimize the production cost. By geometric programming Optimal selection of machining rate variables, was investigated by Petropoulos⁵. A constrained unit cost problem in turning was optimized by using carbide tipped for machining SAE 1045 steel using a goal-programming technique in metal cutting for selecting levels of machining parameters in a fine turning operation on AISI 4140 steel using cemented tungsten carbide tools was studied by Sundaram⁶. constrained multi-pass machining problem was studied by Ermerand Kromodiharajo⁷ and concluded, multi-pass machining was more economical than single-pass machining if depth of cut for each pass was properly allocated. Hinduja⁸ *et al* considered minimum cost or maximum production rate as the objective function and calculated the optimum cutting conditions for turning operation for a given combination of tool and work material, considered surface finish, dimensional accuracy and power available as constraints. Lambert and Taraman⁹ developed a mathematical model to evaluate the cutting force for turning SAE 1018 cold-rolled steel with a carbide tool and utilized the model in the selection of levels of the machining variables such that the material removal rate could be at the highest possible value without violating the given force restrictions. Hassan and Suliman¹⁰ presented mathematical models for the prediction of cutting time, surface roughness, tool vibration, power consumption, while using tungsten carbide tools for turning medium carbon steel under dry conditions. El Baradie¹¹ developed of a surface roughness model while using tipped carbide tools for turning grey cast iron under dry conditions and with constant depth of cut. The mathematical model is utilizing the response surface methodology was developed in terms of cutting speed, feed rate and nose radius of the cutting tool. These variables were investigated using design of experiments and utilization of the response surface methodology. Using of

goal programming technique in for single pass turning operation. T.S. Sidhu¹² determined optimum values for speed and feed by setting different goals for a given set of conditions. Yen and Wright¹³ developed a unified method of adaptive control of constraints in which a suitable cutting region is determined satisfying all the physical constraints. The objective of the optimization is to maximize the production rate under constraints of plastic deformation, crater wear and fracture.

Problem: To find the optimum parameters in order to get the minimum surface roughness and to analyze the effect of machining parameters and rake angles on the surface finish. Design of experiments is the most useful and effective statistical quality control technique to investigate and individual interaction effects of process parameters. It isolates the effect of each input variable. Full factorial experiments consist of possible combinations of the levels of factors. Turning operation was carried out at 3 levels of the back rake, side rake; speed feed and depth of cut the range of parameters are shown in table 1

Table-1
Three levels with five parameters (3⁵ factors design)

| Levels | Rake Angle (°) | | Speed (rpm) | Feed (mm/rev) | Depth of cut (mm) |
|--------|----------------|------|-------------|---------------|-------------------|
| | Back | Side | | | |
| -1 | 8 | 12 | 250 | 0.1 | 0.5 |
| 0 | 11 | 15 | 350 | 0.3 | 1 |
| 1 | 14 | 18 | 550 | 0.5 | 1.5 |

Experimental Procedure: In this work mild steel is selected as the specimen, since it is mostly used structural steel. A mild steel rod of length around 20 ft has taken for this experiment. The lengthy rod was cut into 41 pieces as per required specifications. The Specifications used are ($\phi = 27mm, l = 150mm$) for the specimen with the cutting tool as high speed steel. On each work piece turning operation is performed for three variables like that 243 experiments are conducted on this 41 work pieces. Surface finish is measured using TALYSURF for 243 experiments. Results are tabulated in table 2

Table-2
Surface roughness at various cutting speeds

| S. No. | Rake angle (°) | | Peed (rpm) | Feed (mm/rev) | Doc (mm) | Surface Roughness (μm) |
|--------|----------------|------|------------|---------------|----------|-------------------------------|
| | Back | Side | | | | |
| 1 | 8 | 12 | 250 | 0.1 | 0.5 | 2.835 |
| 2 | 8 | 12 | 250 | 0.1 | 1.0 | 3.190 |
| 3 | 8 | 12 | 250 | 0.1 | 1.5 | 3.510 |
| 4 | 8 | 12 | 250 | 0.3 | 0.5 | 3.810 |
| 5 | 8 | 12 | 250 | 0.3 | 1.0 | 3.405 |
| 6 | 8 | 12 | 250 | 0.3 | 1.5 | 4.390 |
| 7 | 8 | 12 | 250 | 0.5 | 0.5 | 4.270 |
| 8 | 8 | 12 | 250 | 0.5 | 1.0 | 4.210 |
| 9 | 8 | 12 | 250 | 0.5 | 1.5 | 4.410 |

| S. No. | Rake angle (°) | | Peed (rpm) | Feed (mm/rev) | Doc (mm) | Surface Roughness (µm) |
|--------|----------------|----|------------|---------------|----------|------------------------|
| 10 | 8 | 12 | 350 | 0.1 | 0.5 | 2.265 |
| 11 | 8 | 12 | 350 | 0.1 | 1.0 | 2.545 |
| 12 | 8 | 12 | 350 | 0.1 | 1.5 | 2.475 |
| 13 | 8 | 12 | 350 | 0.3 | 0.5 | 3.200 |
| 14 | 8 | 12 | 350 | 0.3 | 1.0 | 3.160 |
| 15 | 8 | 12 | 350 | 0.3 | 1.5 | 3.720 |
| 16 | 8 | 12 | 350 | 0.5 | 0.5 | 4.345 |
| 17 | 8 | 12 | 350 | 0.5 | 1.0 | 3.890 |
| 18 | 8 | 12 | 350 | 0.5 | 1.5 | 4.600 |
| 19 | 8 | 12 | 550 | 0.1 | 0.5 | 2.200 |
| 20 | 8 | 12 | 550 | 0.1 | 1.0 | 1.665 |
| 21 | 8 | 12 | 550 | 0.1 | 1.5 | 2.080 |
| 22 | 8 | 12 | 550 | 0.3 | 0.5 | 2.940 |
| 23 | 8 | 12 | 550 | 0.3 | 1.0 | 2.410 |
| 24 | 8 | 12 | 550 | 0.3 | 1.5 | 2.885 |
| 25 | 8 | 12 | 550 | 0.5 | 0.5 | 3.765 |
| 26 | 8 | 12 | 550 | 0.5 | 1.0 | 3.735 |
| 27 | 8 | 12 | 550 | 0.5 | 1.5 | 4.170 |
| 28 | 8 | 15 | 250 | 0.1 | 0.5 | 3.050 |
| 29 | 8 | 15 | 250 | 0.1 | 1.0 | 2.750 |
| 30 | 8 | 15 | 250 | 0.1 | 1.5 | 3.150 |
| 31 | 8 | 15 | 250 | 0.3 | 0.5 | 3.605 |
| 32 | 8 | 15 | 250 | 0.3 | 1.0 | 3.710 |
| 33 | 8 | 15 | 250 | 0.3 | 1.5 | 3.830 |
| 34 | 8 | 15 | 250 | 0.5 | 0.5 | 4.125 |
| 35 | 8 | 15 | 250 | 0.5 | 1.0 | 4.230 |
| 36 | 8 | 15 | 250 | 0.5 | 1.5 | 5.030 |
| 37 | 8 | 15 | 350 | 0.1 | 0.5 | 2.485 |
| 38 | 8 | 15 | 350 | 0.1 | 1.0 | 2.570 |
| 39 | 8 | 15 | 350 | 0.1 | 1.5 | 2.800 |
| 40 | 8 | 15 | 350 | 0.3 | 0.5 | 3.385 |
| 41 | 8 | 15 | 350 | 0.3 | 1.0 | 2.920 |
| 42 | 8 | 15 | 350 | 0.3 | 1.5 | 3.430 |
| 43 | 8 | 15 | 350 | 0.5 | 0.5 | 3.960 |
| 44 | 8 | 15 | 350 | 0.5 | 1.0 | 4.155 |
| 45 | 8 | 15 | 350 | 0.5 | 1.5 | 4.230 |
| 46 | 8 | 15 | 550 | 0.1 | 0.5 | 2.145 |
| 47 | 8 | 15 | 550 | 0.1 | 1.0 | 2.060 |
| 48 | 8 | 15 | 550 | 0.1 | 1.5 | 2.425 |
| 49 | 8 | 15 | 550 | 0.3 | 0.5 | 2.600 |
| 50 | 8 | 15 | 550 | 0.3 | 1.0 | 2.670 |
| 51 | 8 | 15 | 550 | 0.3 | 1.5 | 3.160 |
| 52 | 8 | 15 | 550 | 0.5 | 0.5 | 3.870 |
| 53 | 8 | 15 | 550 | 0.5 | 1.0 | 3.580 |
| 54 | 8 | 15 | 550 | 0.5 | 1.5 | 4.150 |
| 55 | 8 | 18 | 250 | 0.1 | 0.5 | 2.905 |
| 56 | 8 | 18 | 250 | 0.1 | 1.0 | 2.605 |
| 57 | 8 | 18 | 250 | 0.1 | 1.5 | 3.195 |
| 58 | 8 | 18 | 250 | 0.3 | 0.5 | 3.380 |
| 59 | 8 | 18 | 250 | 0.3 | 1.0 | 3.225 |
| 60 | 8 | 18 | 250 | 0.3 | 1.5 | 3.740 |

| S. No. | Rake angle (°) | | Peed (rpm) | Feed (mm/rev) | Doc (mm) | Surface Roughness (µm) |
|--------|----------------|----|------------|---------------|----------|------------------------|
| 61 | 8 | 18 | 250 | 0.5 | 0.5 | 4.320 |
| 62 | 8 | 18 | 250 | 0.5 | 1.0 | 4.445 |
| 63 | 8 | 18 | 250 | 0.5 | 1.5 | 5.110 |
| 64 | 8 | 18 | 350 | 0.1 | 0.5 | 2.415 |
| 65 | 8 | 18 | 350 | 0.1 | 1.0 | 2.200 |
| 66 | 8 | 18 | 350 | 0.1 | 1.5 | 2.510 |
| 67 | 8 | 18 | 350 | 0.3 | 0.5 | 3.080 |
| 68 | 8 | 18 | 350 | 0.3 | 1.0 | 2.550 |
| 69 | 8 | 18 | 350 | 0.3 | 1.5 | 3.210 |
| 70 | 8 | 18 | 350 | 0.5 | 0.5 | 4.120 |
| 71 | 8 | 18 | 350 | 0.5 | 1.0 | 3.730 |
| 72 | 8 | 18 | 350 | 0.5 | 1.5 | 3.925 |
| 73 | 8 | 18 | 550 | 0.1 | 0.5 | 2.115 |
| 74 | 8 | 18 | 550 | 0.1 | 1.0 | 1.795 |
| 75 | 8 | 18 | 550 | 0.1 | 1.5 | 2.255 |
| 76 | 8 | 18 | 550 | 0.3 | 0.5 | 2.800 |
| 77 | 8 | 18 | 550 | 0.3 | 1.0 | 2.640 |
| 78 | 8 | 18 | 550 | 0.3 | 1.5 | 3.440 |
| 79 | 8 | 18 | 550 | 0.5 | 0.5 | 3.825 |
| 80 | 8 | 18 | 550 | 0.5 | 1.0 | 3.480 |
| 81 | 8 | 18 | 550 | 0.5 | 1.5 | 4.105 |
| 82 | 11 | 12 | 250 | 0.1 | 0.5 | 2.840 |
| 83 | 11 | 12 | 250 | 0.1 | 1.0 | 2.805 |
| 84 | 11 | 12 | 250 | 0.1 | 1.5 | 3.190 |
| 85 | 11 | 12 | 250 | 0.3 | 0.5 | 3.615 |
| 86 | 11 | 12 | 250 | 0.3 | 1.0 | 3.590 |
| 87 | 11 | 12 | 250 | 0.3 | 1.5 | 3.725 |
| 88 | 11 | 12 | 250 | 0.5 | 0.5 | 4.450 |
| 89 | 11 | 12 | 250 | 0.5 | 1.0 | 4.075 |
| 90 | 11 | 12 | 250 | 0.5 | 1.5 | 5.065 |
| 91 | 11 | 12 | 350 | 0.1 | 0.5 | 2.230 |
| 92 | 11 | 12 | 350 | 0.1 | 1.0 | 1.795 |
| 93 | 11 | 12 | 350 | 0.1 | 1.5 | 2.570 |
| 94 | 11 | 12 | 350 | 0.3 | 0.5 | 2.760 |
| 95 | 11 | 12 | 350 | 0.3 | 1.0 | 2.830 |
| 96 | 11 | 12 | 350 | 0.3 | 1.5 | 3.360 |
| 97 | 11 | 12 | 350 | 0.5 | 0.5 | 3.960 |
| 98 | 11 | 12 | 350 | 0.5 | 1.0 | 3.355 |
| 99 | 11 | 12 | 350 | 0.5 | 1.5 | 4.340 |
| 100 | 11 | 12 | 550 | 0.1 | 0.5 | 2.110 |
| 101 | 11 | 12 | 550 | 0.1 | 1.0 | 2.035 |
| 102 | 11 | 12 | 550 | 0.1 | 1.5 | 2.440 |
| 103 | 11 | 12 | 550 | 0.3 | 0.5 | 2.840 |
| 104 | 11 | 12 | 550 | 0.3 | 1.0 | 2.635 |
| 105 | 11 | 12 | 550 | 0.3 | 1.5 | 3.375 |
| 106 | 11 | 12 | 550 | 0.5 | 0.5 | 3.590 |
| 107 | 11 | 12 | 550 | 0.5 | 1.0 | 3.725 |
| 108 | 11 | 12 | 550 | 0.5 | 1.5 | 3.980 |
| 109 | 11 | 15 | 250 | 0.1 | 0.5 | 2.335 |
| 110 | 11 | 15 | 250 | 0.1 | 1.0 | 2.290 |
| 111 | 11 | 15 | 250 | 0.1 | 1.5 | 3.040 |

| S. No. | Rake angle (°) | | Peed (rpm) | Feed (mm/rev) | Doc (mm) | Surface Roughness (µm) |
|--------|----------------|----|------------|---------------|----------|------------------------|
| 112 | 11 | 15 | 250 | 0.3 | 0.5 | 3.480 |
| 113 | 11 | 15 | 250 | 0.3 | 1.0 | 3.405 |
| 114 | 11 | 15 | 250 | 0.3 | 1.5 | 3.780 |
| 115 | 11 | 15 | 250 | 0.5 | 0.5 | 4.725 |
| 116 | 11 | 15 | 250 | 0.5 | 1.0 | 4.410 |
| 117 | 11 | 15 | 250 | 0.5 | 1.5 | 4.850 |
| 118 | 11 | 15 | 350 | 0.1 | 0.5 | 2.145 |
| 119 | 11 | 15 | 350 | 0.1 | 1.0 | 1.925 |
| 120 | 11 | 15 | 350 | 0.1 | 1.5 | 2.480 |
| 121 | 11 | 15 | 350 | 0.3 | 0.5 | 3.210 |
| 122 | 11 | 15 | 350 | 0.3 | 1.0 | 2.940 |
| 123 | 11 | 15 | 350 | 0.3 | 1.5 | 3.220 |
| 124 | 11 | 15 | 350 | 0.5 | 0.5 | 3.795 |
| 125 | 11 | 15 | 350 | 0.5 | 1.0 | 3.640 |
| 126 | 11 | 15 | 350 | 0.5 | 1.5 | 4.440 |
| 127 | 11 | 15 | 550 | 0.1 | 0.5 | 2.040 |
| 128 | 11 | 15 | 550 | 0.1 | 1.0 | 2.110 |
| 129 | 11 | 15 | 550 | 0.1 | 1.5 | 2.260 |
| 130 | 11 | 15 | 550 | 0.3 | 0.5 | 3.040 |
| 131 | 11 | 15 | 550 | 0.3 | 1.0 | 2.560 |
| 132 | 11 | 15 | 550 | 0.3 | 1.5 | 3.080 |
| 133 | 11 | 15 | 550 | 0.5 | 0.5 | 3.220 |
| 134 | 11 | 15 | 550 | 0.5 | 1.0 | 3.375 |
| 135 | 11 | 15 | 550 | 0.5 | 1.5 | 3.900 |
| 136 | 11 | 18 | 250 | 0.1 | 0.5 | 2.815 |
| 137 | 11 | 18 | 250 | 0.1 | 1.0 | 2.600 |
| 138 | 11 | 18 | 250 | 0.1 | 1.5 | 3.275 |
| 139 | 11 | 18 | 250 | 0.3 | 0.5 | 3.440 |
| 140 | 11 | 18 | 250 | 0.3 | 1.0 | 3.250 |
| 141 | 11 | 18 | 250 | 0.3 | 1.5 | 3.870 |
| 142 | 11 | 18 | 250 | 0.5 | 0.5 | 4.465 |
| 143 | 11 | 18 | 250 | 0.5 | 1.0 | 4.210 |
| 144 | 11 | 18 | 250 | 0.5 | 1.5 | 4.700 |
| 145 | 11 | 18 | 350 | 0.1 | 0.5 | 2.350 |
| 146 | 11 | 18 | 350 | 0.1 | 1.0 | 2.475 |
| 147 | 11 | 18 | 350 | 0.1 | 1.5 | 2.580 |
| 148 | 11 | 18 | 350 | 0.3 | 0.5 | 3.345 |
| 149 | 11 | 18 | 350 | 0.3 | 1.0 | 2.580 |
| 150 | 11 | 18 | 350 | 0.3 | 1.5 | 3.555 |
| 151 | 11 | 18 | 350 | 0.5 | 0.5 | 3.750 |
| 152 | 11 | 18 | 350 | 0.5 | 1.0 | 3.740 |
| 153 | 11 | 18 | 350 | 0.5 | 1.5 | 3.825 |
| 154 | 11 | 18 | 550 | 0.1 | 0.5 | 2.040 |
| 155 | 11 | 18 | 550 | 0.1 | 1.0 | 1.880 |
| 156 | 11 | 18 | 550 | 0.1 | 1.5 | 2.280 |
| 157 | 11 | 18 | 550 | 0.3 | 0.5 | 3.170 |
| 158 | 11 | 18 | 550 | 0.3 | 1.0 | 2.205 |
| 159 | 11 | 18 | 550 | 0.3 | 1.5 | 3.215 |
| 160 | 11 | 18 | 550 | 0.5 | 0.5 | 3.425 |
| 161 | 11 | 18 | 550 | 0.5 | 1.0 | 3.440 |
| 162 | 11 | 18 | 550 | 0.5 | 1.5 | 3.815 |

| S. No. | Rake angle (°) | | Peed (rpm) | Feed (mm/rev) | Doc (mm) | Surface Roughness (µm) |
|--------|----------------|----|------------|---------------|----------|------------------------|
| 163 | 14 | 12 | 250 | 0.1 | 0.5 | 2.195 |
| 164 | 14 | 12 | 250 | 0.1 | 1.0 | 2.320 |
| 165 | 14 | 12 | 250 | 0.1 | 1.5 | 3.120 |
| 166 | 14 | 12 | 250 | 0.3 | 0.5 | 3.120 |
| 167 | 14 | 12 | 250 | 0.3 | 1.0 | 3.150 |
| 168 | 14 | 12 | 250 | 0.3 | 1.5 | 3.340 |
| 169 | 14 | 12 | 250 | 0.5 | 0.5 | 4.170 |
| 170 | 14 | 12 | 250 | 0.5 | 1.0 | 3.710 |
| 171 | 14 | 12 | 250 | 0.5 | 1.5 | 4.320 |
| 172 | 14 | 12 | 350 | 0.1 | 0.5 | 2.250 |
| 173 | 14 | 12 | 350 | 0.1 | 1.0 | 1.780 |
| 174 | 14 | 12 | 350 | 0.1 | 1.5 | 2.360 |
| 175 | 14 | 12 | 350 | 0.3 | 0.5 | 2.670 |
| 176 | 14 | 12 | 350 | 0.3 | 1.0 | 2.480 |
| 177 | 14 | 12 | 350 | 0.3 | 1.5 | 3.115 |
| 178 | 14 | 12 | 350 | 0.5 | 0.5 | 3.560 |
| 179 | 14 | 12 | 350 | 0.5 | 1.0 | 3.345 |
| 180 | 14 | 12 | 350 | 0.5 | 1.5 | 3.915 |
| 181 | 14 | 12 | 550 | 0.1 | 0.5 | 1.890 |
| 182 | 14 | 12 | 550 | 0.1 | 1.0 | 1.580 |
| 183 | 14 | 12 | 550 | 0.1 | 1.5 | 1.970 |
| 184 | 14 | 12 | 550 | 0.3 | 0.5 | 2.740 |
| 185 | 14 | 12 | 550 | 0.3 | 1.0 | 2.400 |
| 186 | 14 | 12 | 550 | 0.3 | 1.5 | 2.665 |
| 187 | 14 | 12 | 550 | 0.5 | 0.5 | 3.175 |
| 188 | 14 | 12 | 550 | 0.5 | 1.0 | 2.885 |
| 189 | 14 | 12 | 550 | 0.5 | 1.5 | 3.400 |
| 190 | 14 | 15 | 250 | 0.1 | 0.5 | 2.465 |
| 191 | 14 | 15 | 250 | 0.1 | 1.0 | 2.560 |
| 192 | 14 | 15 | 250 | 0.1 | 1.5 | 2.435 |
| 193 | 14 | 15 | 250 | 0.3 | 0.5 | 3.335 |
| 194 | 14 | 15 | 250 | 0.3 | 1.0 | 2.920 |
| 195 | 14 | 15 | 250 | 0.3 | 1.5 | 3.045 |
| 196 | 14 | 15 | 250 | 0.5 | 0.5 | 3.920 |
| 197 | 14 | 15 | 250 | 0.5 | 1.0 | 3.400 |
| 198 | 14 | 15 | 250 | 0.5 | 1.5 | 4.120 |
| 199 | 14 | 15 | 350 | 0.1 | 0.5 | 1.460 |
| 200 | 14 | 15 | 350 | 0.1 | 1.0 | 1.370 |
| 201 | 14 | 15 | 350 | 0.1 | 1.5 | 2.060 |
| 202 | 14 | 15 | 350 | 0.3 | 0.5 | 2.275 |
| 202 | 14 | 15 | 350 | 0.3 | 1.0 | 2.420 |
| 204 | 14 | 15 | 350 | 0.3 | 1.5 | 2.800 |
| 205 | 14 | 15 | 350 | 0.5 | 0.5 | 3.385 |
| 206 | 14 | 15 | 350 | 0.5 | 1.0 | 3.205 |
| 207 | 14 | 15 | 350 | 0.5 | 1.5 | 3.640 |
| 208 | 14 | 15 | 550 | 0.1 | 0.5 | 1.700 |
| 209 | 14 | 15 | 550 | 0.1 | 1.0 | 1.605 |
| 210 | 14 | 15 | 550 | 0.1 | 1.5 | 1.925 |
| 211 | 14 | 15 | 550 | 0.3 | 0.5 | 2.460 |
| 212 | 14 | 15 | 550 | 0.3 | 1.0 | 2.555 |
| 213 | 14 | 15 | 550 | 0.3 | 1.5 | 2.420 |

| S. No. | Rake angle (°) | | Peed (rpm) | Feed (mm/rev) | Doc (mm) | Surface Roughness (µm) |
|--------|----------------|----|------------|---------------|----------|------------------------|
| 214 | 14 | 15 | 550 | 0.5 | 0.5 | 2.970 |
| 215 | 14 | 15 | 550 | 0.5 | 1.0 | 2.720 |
| 216 | 14 | 15 | 550 | 0.5 | 1.5 | 3.050 |
| 217 | 14 | 18 | 250 | 0.1 | 0.5 | 2.310 |
| 218 | 14 | 18 | 250 | 0.1 | 1.0 | 2.090 |
| 219 | 14 | 18 | 250 | 0.1 | 1.5 | 2.669 |
| 220 | 14 | 18 | 250 | 0.3 | 0.5 | 2.760 |
| 221 | 14 | 18 | 250 | 0.3 | 1.0 | 3.075 |
| 222 | 14 | 18 | 250 | 0.3 | 1.5 | 3.570 |
| 223 | 14 | 18 | 250 | 0.5 | 0.5 | 3.545 |
| 224 | 14 | 18 | 250 | 0.5 | 1.0 | 3.715 |
| 225 | 14 | 18 | 250 | 0.5 | 1.5 | 4.200 |
| 226 | 14 | 18 | 350 | 0.1 | 0.5 | 1.920 |
| 227 | 14 | 18 | 350 | 0.1 | 1.0 | 1.285 |
| 228 | 14 | 18 | 350 | 0.1 | 1.5 | 2.085 |
| 229 | 14 | 18 | 350 | 0.3 | 0.5 | 2.540 |
| 230 | 14 | 18 | 350 | 0.3 | 1.0 | 2.640 |
| 231 | 14 | 18 | 350 | 0.3 | 1.5 | 3.120 |
| 232 | 14 | 18 | 350 | 0.5 | 0.5 | 3.775 |
| 233 | 14 | 18 | 350 | 0.5 | 1.0 | 3.375 |
| 234 | 14 | 18 | 350 | 0.5 | 1.5 | 3.720 |
| 235 | 14 | 18 | 550 | 0.1 | 0.5 | 1.630 |
| 236 | 14 | 18 | 550 | 0.1 | 1.0 | 1.465 |
| 237 | 14 | 18 | 550 | 0.1 | 1.5 | 2.225 |
| 238 | 14 | 18 | 550 | 0.3 | 0.5 | 2.725 |
| 239 | 14 | 18 | 550 | 0.3 | 1.0 | 2.380 |
| 240 | 14 | 18 | 550 | 0.3 | 1.5 | 2.570 |
| 241 | 14 | 18 | 550 | 0.5 | 0.5 | 3.200 |
| 242 | 14 | 18 | 550 | 0.5 | 1.0 | 3.060 |
| 243 | 14 | 18 | 550 | 0.5 | 1.5 | 3.390 |

Results

ANOVA analysis is carried out on the data shown in table1 using MINITAB Software for surface roughness and results are tabulated in table3

Table-3

Analysis of variance for surface roughness

| Source | DF | Seq SS | Adj SS | Adj MS | F | P |
|-----------|-----|--------|--------|--------|-------|------|
| Back Rake | 2 | 12.52 | 12.5 | 6.263 | 155.2 | 8.1 |
| Side Rake | 2 | 0.378 | 0.38 | 0.189 | 4.69 | 0.2 |
| Speed | 2 | 23.69 | 23.7 | 11.84 | 293.6 | 15.3 |
| Feed | 2 | 99.726 | 99.7 | 49.83 | 1236 | 64.3 |
| DOC | 2 | 9.355 | 9.35 | 4.677 | 115.9 | 6.05 |
| Error | 232 | 9.359 | 9.35 | 0.040 | | 6.05 |
| Total | 242 | 155.03 | | | | |

S = 0.200851 R-Sq = 93.96% R-Sq(adj) = 93.70%

Main effects plot and interaction plot are shown in figure .2 and figure-3

Conclusion

From figure-2it is observed that minimum surface roughness is obtained at a speed of 550 rpm, feed of 0.1 mm/rev, depth of cut of 1mm, side rake angle of 18° and back rake angle of 14° the surface finish is 1.465µm.

From table3 it is observed that feed is the significant parameter influencing surface roughness and side rake angle is having very less effect on surface roughness

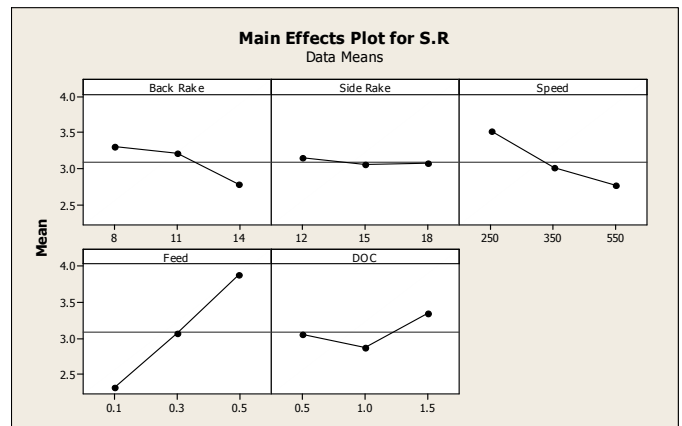


Figure-2
Main Effects Plot



Figure-3
Interaction Plot

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